

The roughening transition of vicinal surfaces

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Abstract. Facetting of a vicinal surface is due to an arrangement of parallel primary steps which is commensurate with the substrate in plane periodicity (for instance one step every p th atomic row). It was shown by [4] that such a locking requires an interaction between steps together with a finite step stiffness. But this early approach only reveals part of the story, as it is limited to sharp solid-vacuum interfaces in which thermal excitation of energetically expensive kinks controls all fluctuations. In this paper the problem is taken afresh in a language which applies equally well to “soft” interfaces, with important changes in the conclusions.

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The roughening transition of a regular facet $z = 0$ is a compromise between the capillary energy of the interface and a periodic pinning potential with a period a along the normal z axis. At low temperatures small terraces are bounded by sharp steps. Beyond a critical temperature T_R these terraces coalesce, and steps span the whole width of the interface, which becomes rough. Such a transition has been widely studied [2, 3]: it is dual to a $2d$ (X, Y) model (the role of low and high temperatures are interchanged). A similar facetting occurs for vicinal surfaces, in which a regular array of parallel steps with distance d acts to tilt the interface. Although in the same universality class as for a regular facet, such a transition is somewhat different, as it corresponds to a *commensurate* arrangement of d with the lattice spacing b along the plane. That problem was studied long ago [4] in the case of solid-vacuum interfaces, for which steps and kinks are essentially atomic entities. The step energy then dominates everything and the roughening temperature T_R is close to the kink energy ε within logarithmic corrections. The situation is different for broad steps as befits a solid-liquid interface. We take that problem afresh, using the same approach for both limits, and we show that T_R rapidly decreases as d grows. We thus complement the pioneering work of [4].

1 Properties of a planar facet

They were discussed long time ago, for instance by the author in [1]. Consider the (100) facet of an orthorhombic crystal. In a first approximation we ignore the periodicity in the (x, y) plane of the interface: the crystal is a stack of

structureless plates. The lattice spacing in the normal z direction is a . We describe the surface distortions within a simple continuous model $z(x, y)$, corresponding to an energy (at finite temperature “energy” means “free energy”)

$$E = \int dx dy \left[\frac{\gamma}{2} (\text{grad } z)^2 + V \cos \frac{2\pi z}{a} \right] \quad (1)$$

γ is a surface tension, V a potential that pins the surface onto crystal planes. We assume that V is small, as might be the case at a solid-liquid interface. At zero temperature T , such a model allows for “solitons” that connect planar regions $z = 0$ and $z = a$: these are the *crystal steps* of the facet, with a width $\xi_0 \approx a\sqrt{\gamma/V}$ and an energy per unit length $\beta_0 \approx a\sqrt{\gamma V}$. Note that $\beta_0 \xi_0 \approx \gamma a^2$. At this stage β does not depend on the azimuth φ of the step in the (x, y) plane.

For an unpinning surface ($V = 0$), thermal fluctuations follow from equipartition of each Fourier component, $\overline{z_k^2} = T/\gamma k^2$. The net fluctuations of the local amplitude z are Gaussian, given by

$$\overline{z^2} = \frac{1}{4\pi^2} \int 2\pi k dk \frac{T}{\gamma k^2} = \frac{T}{2\pi\gamma} \text{Log} \frac{L}{\xi}. \quad (2)$$

The upper and lower cutoffs are respectively the width L of the facet and the step width ξ . When the periodic potential V is restored, it couples fluctuation modes with different k – hence the difficulty. The *roughening transition* at $T = T_R$ separates a high temperature “rough” state in which fluctuations of z diverge logarithmically, from a low temperature faceted state in which they are

bounded. As shown in [1], a very simple argument yields T_R in lowest order in V : we need only calculate the *first order* average pinning energy U of an $L \times L$ square, which requires the *zeroth order* fluctuations of z :

$$U = VL^2 \cos \frac{2\pi z}{a} = L^2 V \exp \left[-\frac{2\pi^2 z^2}{a^2} \right].$$

Using (2), we obtain

$$U = VL^2 \left(\frac{\xi}{L} \right)^{\pi T / \gamma a^2}.$$

Hence two situations:

(i) if $T > \frac{2}{\pi} \gamma a^2$, the power of L is negative: pinning is less and less relevant as the scale L grows, the surface is macroscopically free, hence rough.

(ii) if $T < \frac{2}{\pi} \gamma a^2$ the power is positive: pinning is more and more efficient. Fluctuations stop when $U \approx T$, which defines a characteristic length $L \approx \xi$ – the width of the crystal step.

The roughening transition occurs at

$$T_R = \frac{2}{\pi} \gamma a^2. \quad (3)$$

Such a naive calculation is only exact in first order in V . It holds in all cases if γ is taken to be the surface *free energy* at T_R instead of the original $T = 0$ energy (in the renormalization approach of Kosterlitz and Thouless, fixed point properties correspond to $V = 0$). For weak pinning fancy methods are not necessary in order to find T_R – in contrast they are crucial in finding critical behaviour *near* the transition.

2 Facetting of a vicinal surface

We now tilt the interface: the normal stays in the (z, x) plane and it is rotated by a small angle θ . We denote by (x, y, z) coordinates referred to the crystal planes, by (\bar{x}, y, \bar{z}) those referred to the average surface. Well separated steps parallel to the y axis appear if $\theta \ll a/\xi$: we restrict ourselves to such a *vicinal* regime. The step distance along the x axis is d , such that $\tan \theta = a/d$. The surface energy per unit length dx may be written as

$$E(n) = \gamma_0 + \beta n + E_{\text{int}}(n)$$

$n = 1/d$ is the step density, γ_0 the perfect facet surface energy, β the step energy, E_{int} their interaction, whatever their origin (entropic, elastic, electrostatic...). All known mechanisms yield a $1/d^2$ repulsion: we thus write $E_{\text{int}}(n) = \lambda n^3$, where λ is an *ad hoc* coefficient. Since the surface length $d\bar{x} = dx / \cos \theta$, it follows that the surface energy of the vicinal surface is $\gamma(\theta) = E(n) \cos \theta$. All the physics lies in $E(n)$ – for instance the equilibrium shape.

A vicinal surface is always rough if there is no periodicity inside the crystal planes: for such a stack of structureless plates steps can slide freely along the interface. Whenever a step sweeps by a given point M , the height shifts

by $\pm a$, hence random fluctuations that produce the logarithmic divergence of a free surface (albeit with a much reduced amplitude). The only way to avoid roughness is to lock the steps onto an underlying periodicity in the x direction: a faceted state is then a *commensurate arrangement of steps*, arising from a combination of periodicity and step interactions. The roughening transition is the loss of that commensurability due to thermal fluctuations. We consider only the very simplest case of a $(1, 0, p)$ facet: a step appears every p th row in the x direction, so that the step distance $d = pb$, where b is the lattice spacing along the x axis. Assuming $b \neq a$ allows a clear identification of the roles played by the two periodicities. Our goal is to find the roughening temperature $T_R(p)$ of such a higher order facet using the same naive argument introduced for the original $(0, 0, 1)$ facet. In that way we do not use specific details of the commensurate structure: the only information we need is the “stiffness” γ_{eff} of the vicinal surface, and the “period” a_{eff} along the normal \bar{x} to the real surface. Using (3) we obtain at once $T_R(p)$.

It is clear that a vicinal surface is anisotropic. Let us consider a fluctuation $\bar{z}(\bar{x}, y)$ with wave vector (k_x, k_y) : the corresponding cost in energy may be written as

$$dU = \frac{1}{2} [\tilde{\gamma}_x k_x^2 + \tilde{\gamma}_y k_y^2] \bar{z}^2 d\bar{x}$$

$\tilde{\gamma}$ is the effective *surface stiffness* that controls surface deformations. Fluctuations with a wave vector k_x perpendicular to the step correspond to a *compression wave* of the latter: $\tilde{\gamma}_x$ is due only to step interactions, according to

$$dU = \frac{1}{2} E''(n) \delta n^2 dx = \frac{1}{2} E'' \frac{\delta \theta^2}{a^2 \cos^3 \theta} d\bar{x}.$$

Equating the two expressions of δU yields

$$\tilde{\gamma}_x = \frac{6\lambda \tan \theta}{a^3 \cos^3 \theta}. \quad (4)$$

In contrast fluctuations with wave vector k_y correspond to an *undulation wave* of steps, with three distinct effects:

(i) Steps are *lengthened*, by a factor

$$\left[1 + \frac{1}{2} \left(\frac{\partial \delta u}{\partial y} \right)^2 \right]$$

where $\delta u(y)$ is the local displacement of the steps along the x axis.

(ii) They are *rotated* by an angle $\delta \phi = \partial \delta u / \partial y$, which in turn affects their energy $\beta(\phi)$ (periodicity in the (x, y) plane means loss of rotational invariance: the step parameters β and λ depend on the azimuthal angle ϕ). The joint energy cost of lengthening and rotation may be written as

$$dU = \frac{1}{2} \tilde{\beta} k_y^2 \delta u^2 n dx$$

where $\tilde{\beta} = \beta + \beta''$ is the “step stiffness”, which must be positive for the step to be stable. Strictly speaking the single step energy β should be replaced by the full energy

per step, E/n , which includes the interaction with neighbours: for simplicity we assume that n is small enough for that correction to be negligible.

(iii) Finally the distance between steps is reduced from d to $d \cos \delta\phi$, which affects their interaction. But we just neglected that interaction energy when compared to the bare β : in order to be consistent we should also ignore the correction due to δd . Note that including these effects is straightforward if needed!

In order to transform these data into a $\tilde{\gamma}_y$, we note that each step which sweeps by a given x raises z by a , from which we infer $\delta z = na \delta u$. Since dU is also

$$dU = \frac{1}{2} \tilde{\gamma}_y k_y^2 \delta \bar{z}^2 d\bar{x} = \frac{1}{2} \tilde{\gamma}_y k_y^2 \delta z^2 \cos^2 \theta \frac{dx}{\cos \theta}$$

we finally obtain

$$\tilde{\gamma}_y = \frac{\tilde{\beta}}{a \sin \theta}. \tag{5}$$

What matters for us is the mean square fluctuation of \bar{z} in the absence of inplane periodicity

$$\overline{z^2} = \frac{1}{4\pi^2} \int dk_x dk_y \frac{T}{\gamma_x k_x^2 + \gamma_y k_y^2}.$$

Stiffness only enters through the combination

$$\gamma_{\text{eff}} = \sqrt{\gamma_x \gamma_y} = \frac{\sqrt{6\lambda\tilde{\beta}}}{a^2 \cos^2 \theta}. \tag{6}$$

The results (4) to (6) are well known (see for instance [1]): we rederive them in order to emphasize the underlying physics. Note that γ_{eff} is nearly constant for a small tilt angle θ : the large variations of γ_x and γ_y cancel out.

We finally need a_{eff} : by definition it is the smallest distance along the \bar{z} axis after which the same surface energy is recovered. It corresponds to a translation by a lattice spacing b in the x direction, not along the z axis. It follows that

$$a_{\text{eff}} = b \sin \theta = \frac{a \cos \theta}{p}. \tag{7}$$

Using (3) we obtain a very simple result for the roughening temperature

$$T_R = \frac{2}{\pi} \frac{\sqrt{6\lambda\tilde{\beta}}}{p^2}. \tag{8}$$

That expression (8) is the central result of this paper. It relies on two approximations, one minor (corrections to λ and $\tilde{\beta}$ can easily be included), the other one more fundamental (we use zero temperature properties instead of fixed point quantities at T_R). Basically we assume that scaling does not renormalize γ_{eff} too much. Let us emphasize again that (7) and (8) are the only new features in our argument: they build on existing knowledge.

Note that faceting depends crucially on step interaction, as surmised correctly by [4]: without interactions a given step would necessarily wander and commensurate locking could not occur! A question then comes naturally

to one's mind: can a purely entropic repulsion lead to faceting? A positive answer would be surprising, since more entropy could hardly be expected to produce order! Indeed it cannot occur! The entropic repulsion has been calculated exactly by [5] (the original calculation of [6], using a mapping on a free fermion gas, is off by a factor 2). One thus finds

$$\lambda = \frac{\pi^2 T^2}{6\tilde{\beta}}.$$

When inserted into (8) that would lead to (9)

$$T_R = T \frac{2}{p^2} \tag{9}$$

(note that the step stiffness $\tilde{\beta}$ disappears), a condition that can never be met for the large p of a vicinal surface. A standard roughening transition triggered by entropic step interaction is thus impossible. Only genuine mechanical interactions can do the job, as shown by [7].

3 Comparison with the results for solid vacuum interfaces

According to (8), T_R goes to 0 as the index of the vicinal surface grows. Such a conclusion looks dramatically different from that of [4], who claim that T_R is always close to the kink energy ε : why? The answer to that question sits in the stiffness parameter $\tilde{\beta}$. While the elastic interaction λ does not depend much on the nature of the interface, the stiffness $\tilde{\beta}$ is much larger for the narrow steps of a vacuum interface than it would be for the broad steps of a liquid interface. Qualitatively, the only way to make a step wander is to create kinks, and sharp kinks cost energy! The resulting Boltzmann factor leads to a fast increase of $\tilde{\beta}$ at low temperatures, which dominates everything else.

In order to make that handwaving argument precise, we first define kinks and we calculate the step stiffness directly. A tilted single step develops localized kinks, who have an energy ε of atomic scale. The kink width ζ along the step is such that $\varepsilon\zeta \approx \beta b^2$ (in an atomic picture ζ is the lattice spacing c along the y axis). At any finite temperature there exists a finite density of kinks

$$n_K = \frac{\exp(-\varepsilon/T)}{\zeta}.$$

Two situations may then hold:

(i) $T \gtrsim \varepsilon$: thermal kinks are numerous, the step moves freely. The anisotropy of $\beta(\phi)$ is not dramatic and $\tilde{\beta}$ is comparable to the step energy β . The result (8) should then hold as such.

(ii) $T \ll \varepsilon$: step fluctuations depends on the displacement of a few kinks and the step is far stiffer. $\tilde{\beta}$ is easily found calculating the step correlation function

$$G(y) = \overline{[x(y) - x(0)]^2}$$

for large y in two ways. On a macroscopic scale

$$G = \frac{1}{\pi} \int_0^\infty dk \frac{T}{\tilde{\beta} k^2} 2(1 - \cos ky) = \frac{T y}{\tilde{\beta}}.$$

On the kink scale, kinks are of either sign, leftward or rightward, and step fluctuations are due to a local excess of kinks of one type. A length y of step contains $N = n_K y/c$ kinks, and standard combinatorics yields $G(y) = Nb^2$. It follows that

$$\tilde{\beta} = \frac{Tc}{b^2} \exp(\varepsilon/T). \quad (10)$$

Carrying (10) into (8) we see that the roughening temperature is a solution to

$$\exp(\varepsilon/T) = \frac{\pi^2}{24} \frac{p^4 b^2 T}{\lambda \zeta}. \quad (11)$$

That should be compared with the result [4] which reads

$$\exp(\varepsilon/T) = \frac{2T}{W_p} \quad (12)$$

W_p is the second derivative of the step interaction energy on a length ζ

$$W_p = \lambda \zeta \left[\frac{1}{(d+b)^2} + \frac{1}{(d-b)^2} - \frac{2}{d^2} \right] \approx \frac{6\lambda \zeta}{p^4 b^2}.$$

In practice the two results agree in that limit, but for numerical factors!

In such an ‘‘atomic limit’’, what matters is the value of ε . A roughening temperature cannot be much smaller than ε : if it were the stiffness $\tilde{\beta}$ would increase exponentially, thereby blocking fluctuations. In the opposite limit of a small ε the stiffness does not vary much with temperature: the behaviour predicted by (8) is then clearly apparent (if p increases one always returns to the strong coupling limit). It is interesting, however, to note that (8) is always valid: the $1/p^2$ behaviour is just hidden when $\tilde{\beta}$ is calculated in the strong coupling limit!

Our conclusion is that the roughening transition of vicinal surfaces provides a useful test of step interactions, with one caveat: the result of [4] holds only for sharp vacuum interfaces, and it should not be used inconsiderately.

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